

# Zero-Drift, Low Power, CMOS Operational Amplifiers

## 1 FEATURES

- **Input Offset Voltage:  $\pm 7\mu\text{V}$  (TYP)**
- **Input Offset Drift:  $\pm 0.08\mu\text{V}/^\circ\text{C}$**
- **Low Quiescent Current:  $40\mu\text{A}/\text{Amp}$**
- **Gain Bandwidth:  $350\text{kHz}$**
- **Rail to Rail Input and Output**
- **Low Noise:  $0.9\mu\text{V}_{\text{P-P}}$  (0.1Hz to 10Hz)**
- **Slew Rate:  $0.16\text{V}/\mu\text{s}$**
- **Supply Range: 2V to 5.5V**
- **Extended Temperature:  $-40^\circ\text{C}$  to  $+125^\circ\text{C}$**
- **Micro SIZE PACKAGES: SOT23-5, SOP8**

## 2 APPLICATIONS

- **Battery Powered Instruments**
- **Medical Instruments**
- **Handheld Test Equipment**
- **Temperature Measurements**
- **Transducers**
- **Electronic Scales**

## 3 DESCRIPTIONS

The RS8541, RS8542 series of CMOS operational amplifiers use auto-calibration techniques to simultaneously provide very low offset voltage ( $7\mu\text{V}$  TYP) and near-zero drift over time and temperature. This family of amplifiers has ultralow noise, offset and power.

This miniature, high-precision operational amplifiers offset high input impedance and rail-to-rail input and rail-to-rail output swing. With gain-bandwidth product of  $350\text{kHz}$  and slew rate of  $0.16\text{V}/\mu\text{s}$ . Single or dual supplies as low as  $+2\text{V}$  ( $\pm 1\text{V}$ ) and up to  $+5.5\text{V}$  ( $\pm 2.75\text{V}$ ) may be used.

The RS854X are specified for the extended industrial and automotive temperature range ( $-40^\circ\text{C}$  to  $125^\circ\text{C}$ ). The RS8541 single amplifier is available in 5-lead SOT23 package, The RS8542 dual amplifier is available in 8-lead SOP package.

**Device Information <sup>(1)</sup>**

PART NUMBER	PACKAGE	BODY SIZE(NOM)
RS8541	SOT23-5	$2.92\text{mm} \times 1.60\text{mm}$
RS8542	SOP8	$4.90\text{mm} \times 3.90\text{mm}$

(1) For all available packages, see the orderable addendum at the end of the data sheet.

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## 4 REVISION HISTORY

Note: Page numbers for previous revisions may differ from page numbers in the current version.

<b>VERSION</b>	<b>Change Date</b>	<b>Change Item</b>
A.0	2023/06/13	Preliminary version completed
A.1	2023/08/24	Initial version completed
A.1.1	2024/03/01	Modify packaging naming
A.2	2024/12/24	1. Delete RS8541BXC5/RS8542XM Orderable Device 2. Add MSL on Page 4 in RevA.1.1

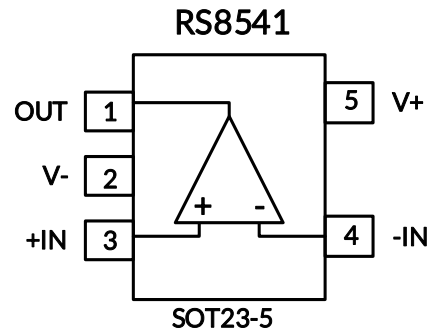
**5 PACKAGE/ORDERING INFORMATION <sup>(1)</sup>**

Orderable Device	Package Type	Pin	Channel	Op Temp(°C)	Device Marking <sup>(2)</sup>	MSL <sup>(3)</sup>	Package Qty
RS8541XF	SOT23-5	5	1	-40°C ~125°C	8541	MSL3	Tape and Reel,3000
RS8542XK	SOP8	8	2	-40°C ~125°C	RS8542	MSL3	Tape and Reel,4000

## NOTE:

- (1) This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the right-hand navigation.
- (2) There may be additional marking, which relates to the lot trace code information (data code and vendor code), the logo or the environmental category on the device.
- (3) RUNIC classify the MSL level with using the common preconditioning setting in our assembly factory conforming to the JEDEC industrial standard J-STD-20F. Please align with RUNIC if your end application is quite critical to the preconditioning setting or if you have special requirement.

## 6 PIN CONFIGURATION AND FUNCTIONS

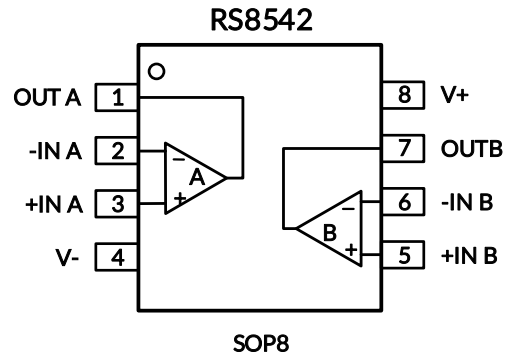


### Pin Description

NAME	PIN		I/O <sup>(1)</sup>	DESCRIPTION
	RS8541			
	SOT23-5			
-IN	4	I	Negative (inverting) input	
+IN	3	I	Positive (noninverting) input	
OUT	1	O	Output	
V-	2	-	Negative (lowest) power supply	
V+	5	-	Positive (highest) power supply	

(1) I = Input, O = Output.

## PIN CONFIGURATION AND FUNCTIONS



### Pin Description

NAME	PIN		I/O <sup>(1)</sup>	DESCRIPTION
	RS8542			
	SOP8			
-INA	2		I	Inverting input, channel A
+INA	3		I	Noninverting input, channel A
-INB	6		I	Inverting input, channel B
+INB	5		I	Noninverting input, channel B
OUTA	1		O	Output, channel A
OUTB	7		O	Output, channel B
V-	4		-	Negative (lowest) power supply
V+	8		-	Positive (highest) power supply

(1) I = Input, O = Output.

## 7 SPECIFICATIONS

### 7.1 Absolute Maximum Ratings

Over operating free-air temperature range (unless otherwise noted) <sup>(1)</sup>

		MIN	MAX	UNIT
Voltage	Supply, $V_S=(V+) - (V-)$		7	V
	Signal input pin <sup>(2)</sup>	(V-)-0.3	(V+) +0.3	
	Signal output pin <sup>(3)</sup>	(V-)-0.3	(V+) +0.3	
Current	Signal input pin <sup>(2)</sup>	-10	10	mA
	Signal output pin <sup>(3)</sup>	-10	10	mA
	Output short-circuits <sup>(4)</sup>	Continuous		
$\theta_{JA}$	Package thermal impedance <sup>(5)</sup>	SOT23-5	230	°C/W
		SOP8	110	
Temperature	Operating range, $T_A$	-40	125	°C
	Junction, $T_J$ <sup>(6)</sup>	-40	150	
	Storage, $T_{stg}$	-65	150	

(1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not implied.

(2) Input terminals are diode-clamped to the power-supply rails. Input signals that can swing more than 0.3V beyond the supply rails should be current-limited to 10mA or less.

(3) Output terminals are diode-clamped to the power-supply rails. Output signals that can swing more than 0.3V beyond the supply rails should be current-limited to  $\pm 10$ mA or less.

(4) Short-circuit to ground, one amplifier per package.

(5) The package thermal impedance is calculated in accordance with JESD-51.

(6) The maximum power dissipation is a function of  $T_{J(MAX)}$ ,  $R_{\theta JA}$ , and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} - T_A) / R_{\theta JA}$ . All numbers apply for packages soldered directly onto a PCB.

### 7.2 ESD Ratings

The following ESD information is provided for handling of ESD-sensitive devices in an ESD protected area only.

			VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human-Body Model (HBM), MIL-STD-883K METHOD 3015.9	$\pm 4000$	V
		Charged-Device Model (CDM), ANSI/ESDA/JEDEC JS-002-2018	$\pm 1000$	
		Machine Model (MM), JESD22-A115C (2010)	$\pm 300$	



#### ESD SENSITIVITY CAUTION

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### 7.3 Recommended Operating Conditions

Over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
Supply voltage, $V_S=(V+) - (V-)$	Single-supply	2		5.5	V
	Dual-supply	$\pm 1$		$\pm 2.75$	
Specified temperature		-40		125	°C

## 7.4 Electrical Characteristics

Boldface limits apply over the specified temperature range, Full <sup>(9)</sup> = -40°C to +125°C.

(At  $T_A = +25^\circ\text{C}$ ,  $V_S = 5\text{V}$ ,  $R_L = 10\text{k}\Omega$  connected to  $V_S/2$ , and  $V_{\text{OUT}} = V_S/2$ ,  $V_{\text{CM}} = V_S/2$ , unless otherwise noted.) <sup>(1)</sup>

PARAMETER		CONDITIONS	RS854X			
			MIN <sup>(2)</sup>	TYP <sup>(3)</sup>	MAX <sup>(2)</sup>	UNIT
<b>POWER SUPPLY</b>						
$V_S$	Operating Voltage Range		2		5.5	V
$I_Q$	Quiescent Current Per Amplifier			40	60	$\mu\text{A}$
PSRR	Power-Supply Rejection Ratio	$V_S = 2\text{V to } 5.5\text{V}$	95	110		dB
<b>INPUT</b>						
$V_{\text{OS}}$	Input Offset Voltage	$V_S = 2\text{V}, V_{\text{CM}} = V_S/2$	-30	$\pm 3$	30	$\mu\text{V}$
		$V_S = 5\text{V}, V_{\text{CM}} = V_S/2$	-30	$\pm 7$	30	$\mu\text{V}$
$V_{\text{OS Tc}}$	Input Offset Voltage Average Drift			$\pm 0.08$		$\mu\text{V}/^\circ\text{C}$
IB	Input Bias Current <sup>(4)(5)</sup>	$V_{\text{CM}} = V_S/2$		$\pm 330$		pA
$I_{\text{OS}}^{(5)}$	Input Offset Current	$V_{\text{CM}} = V_S/2$		$\pm 100$		pA
$V_{\text{CM}}$	Common-Mode Voltage Range		$(V_-) - 0.1$		$(V_+) + 0.1$	V
CMRR	Common-Mode Rejection Ratio	$(V_-) - 0.1\text{V} < V_{\text{CM}} < (V_+) + 0.1\text{V}$	105	120		dB
<b>INPUT CAPACITANCE</b>						
	Differential <sup>(5)</sup>			2.5		pF
	Common-Mode <sup>(5)</sup>			5		pF
<b>OUTPUT</b>						
$A_{\text{OL}}$	Open-Loop Voltage Gain	$R_L = 10\text{k}\Omega$ , $V_O = 0.3\text{V to } 4.7\text{V}$	105	130		dB
$V_{\text{OL}}$	Output Voltage Low from rail	$R_L = 100\text{ k}\Omega$ to GND		1		mV
		$R_L = 10\text{ k}\Omega$ to GND		10	20	
$V_{\text{OH}}$	Output Voltage High from rail	$R_L = 100\text{ k}\Omega$ to $V_+$		1		mV
		$R_L = 10\text{ k}\Omega$ to $V_+$		10	20	
$I_{\text{SC}}$	Output Short-Circuit Current <sup>(6)(7)</sup>		$\pm 20$	$\pm 30$		mA
<b>FREQUENCY RESPONSE</b>						
SR	Slew Rate <sup>(8)</sup>	$G = +1$		0.16		$\text{V}/\mu\text{s}$
GBW	Gain-Bandwidth Product			350		KHz
$t_{\text{OR}}$	Overload Recovery Time	$V_{\text{IN}} \cdot \text{Gain} \geq V_S$		3		$\mu\text{s}$
<b>NOISE PERFORMANCE</b>						
$e_{\text{n p-p}}$	Input Voltage Noise	$f = 0.1\text{Hz to } 10\text{Hz}$		0.9		$\mu\text{V}_{\text{PP}}$
$e_{\text{n p-p}}$	Input Voltage Noise <sup>(5)</sup>	$f = 0.01\text{Hz to } 1\text{Hz}$		0.25		$\mu\text{V}_{\text{PP}}$
$e_{\text{n}}$	Input Voltage Noise Density <sup>(5)</sup>	$f = 1\text{KHz}$		45		$\text{nV}/\sqrt{\text{Hz}}$

NOTE:

- (1) Electrical table values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device.
- (2) Limits are 100% production tested at 25°C. Limits over the operating temperature range are ensured through correlations using statistical quality control (SQC) method.
- (3) Typical values represent the most likely parametric norm as determined at the time of characterization. Actual typical values may vary over time and will also depend on the application and configuration.
- (4) Positive current corresponds to current flowing into the device.
- (5) This parameter is ensured by design and/or characterization and is not tested in production.
- (6) The maximum power dissipation is a function of  $T_{\text{J(MAX)}}$ ,  $R_{\theta\text{JA}}$ , and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $\text{PD} = (T_{\text{J(MAX)}} - T_A) / R_{\theta\text{JA}}$ . All numbers apply for packages soldered directly onto a PCB.
- (7) Short circuit test is a momentary test.
- (8) Number specified is the slower of positive and negative slew rates.
- (9) Specified by characterization only.



### 7.5 Typical Characteristics

NOTE: The graphs and tables provided following this note are a statistical summary based on a limited number of samples and are provided for informational purposes only.

At  $T_A = +25^\circ\text{C}$ ,  $V_S=5\text{V}$ ,  $R_L = 10\text{k}\Omega$  connected to  $V_S/2$ ,  $V_{OUT} = V_S/2$ , unless otherwise noted.

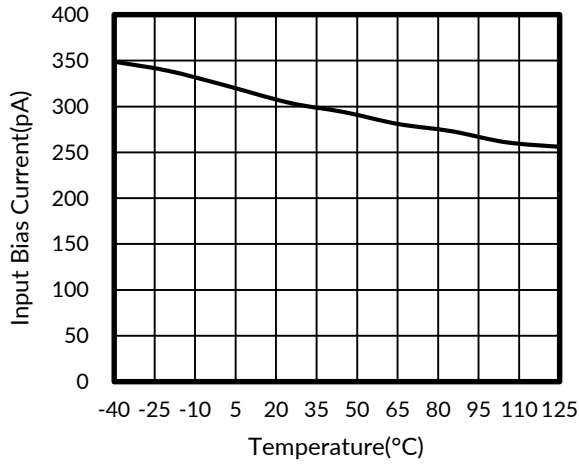


Figure 1. Input Bias Current vs Temperature

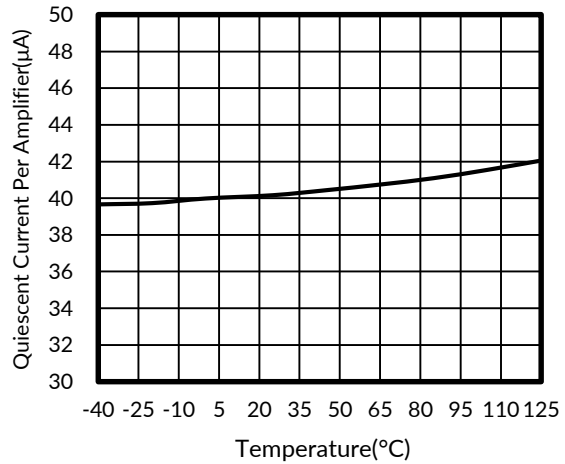


Figure 2. Quiescent Current vs Temperature

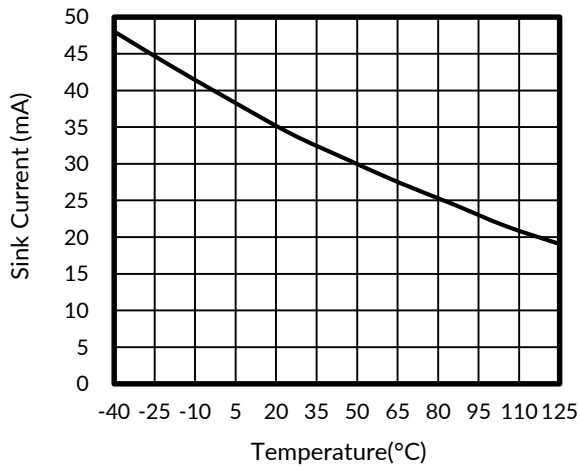


Figure 3. Sink Current vs Temperature

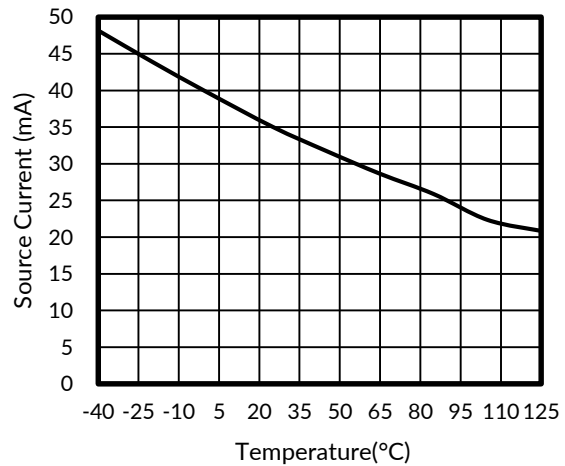


Figure 4. Source Current vs Temperature

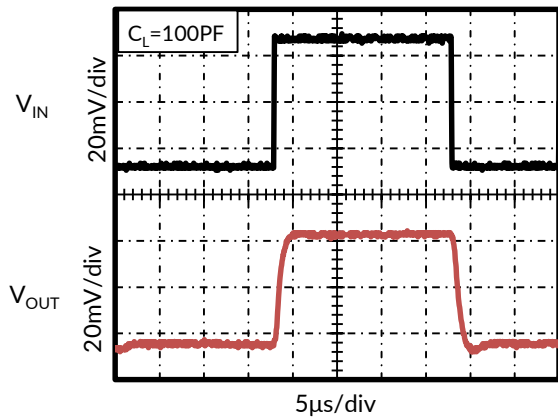


Figure 5. Small-Signal Step Response

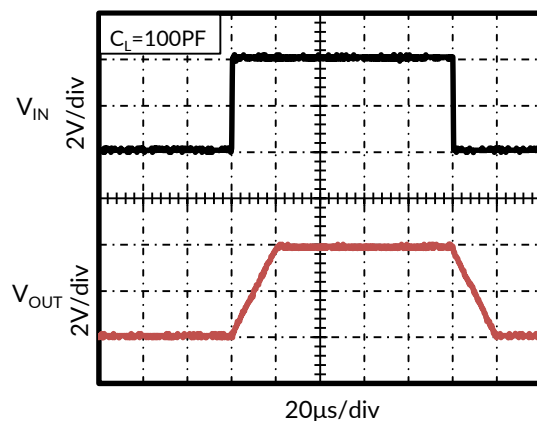
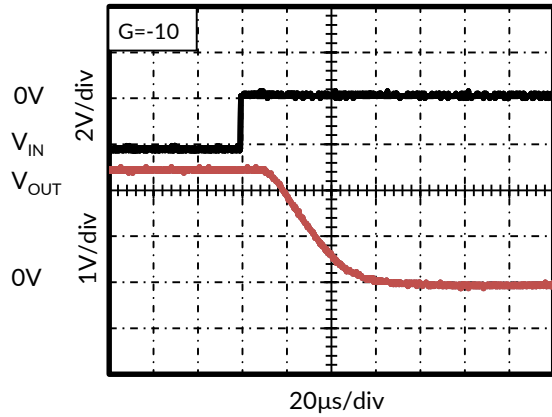


Figure 6. Large-Signal Step Response

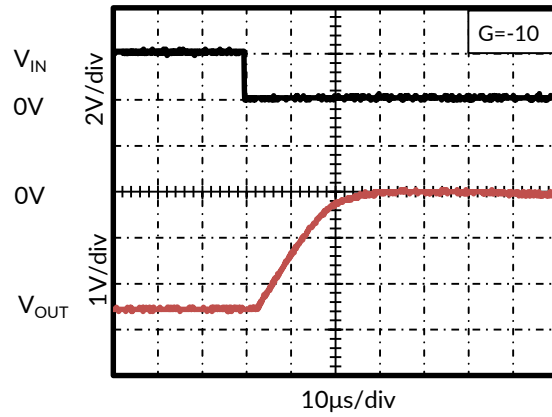
## Typical Characteristics

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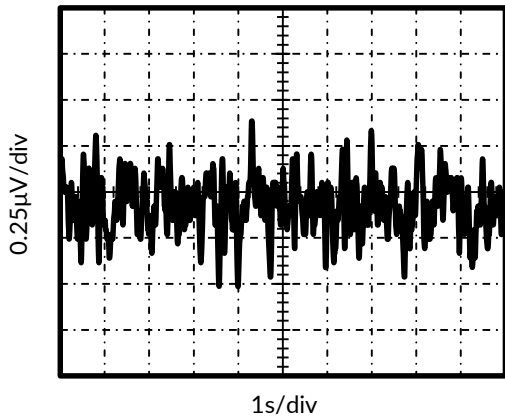
At  $T_A = +25^\circ\text{C}$ ,  $V_S = 5\text{V}$ ,  $R_L = 10\text{k}\Omega$  connected to  $V_S/2$ ,  $V_{OUT} = V_S/2$ , unless otherwise noted.



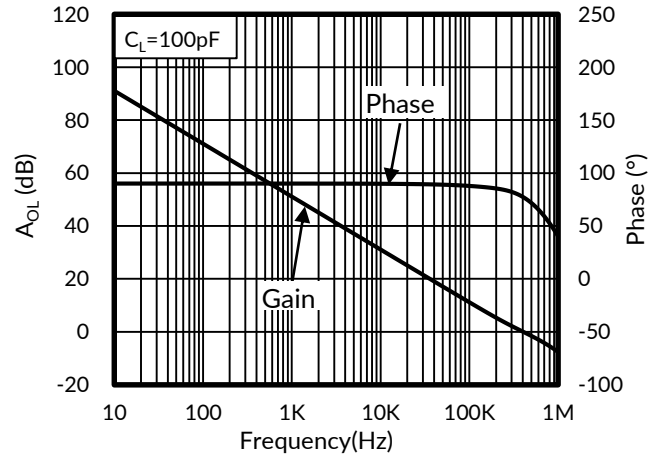
**Figure 7. Positive Overvoltage Recovery**



**Figure 8. Negative Overvoltage Recovery**



**Figure 9. 0.1Hz to 10Hz Noise**



**Figure 10. Open-Loop Gain and Phase vs Frequency**

## 8 DETAILED DESCRIPTION

### 8.1 Overview

The RS854X is a family of Zero-Drift, low-power, rail-to-rail input and output operational amplifiers. These devices operate from 2 V to 5.5 V, are unity-gain stable, and are suitable for a wide range of general-purpose applications. The Zero-Drift architecture provides ultra low offset voltage and near-zero offset voltage drift.

### 8.2 Feature Description

The RS854X series op amps are unity-gain stable and free from unexpected output phase reversal. They use auto-zeroing techniques to provide low offset voltage and very low drift over time and temperature.

Good layout practice mandates use of a 0.1 $\mu$ F capacitor placed closely across the supply pins.

For lowest offset voltage and precision performance, circuit layout and mechanical conditions should be optimized. Avoid temperature gradients that create thermoelectric (Seebeck) effects in thermocouple junctions formed from connecting dissimilar conductors. These thermally-generated potentials can be made to cancel by assuring that they are equal on both input terminals.

- Use low thermoelectric-coefficient connections (avoid dissimilar metals).
- Thermally isolate components from power supplies or other heat-sources.
- Shield op amp and input circuitry from air currents, such as cooling fans.

Following these guidelines will reduce the likelihood of junctions being at different temperatures, which can cause thermoelectric voltages of 0.1 $\mu$ V/ $^{\circ}$ C or higher, depending on materials used.

### 8.3 Operating Voltage

The RS854X series op amps operate over a power-supply range of +2V to +5.5V ( $\pm$ 1V to  $\pm$ 2.75V). Supply voltages higher than 7V (absolute maximum) can permanently damage the amplifier. Parameters that vary over supply voltage or temperature are shown in the Typical Characteristics section of this data sheet.

### 8.4 Device Functional Modes

The RS854X device has a single functional mode. The device is powered on as long as the power supply voltage is between 2 V ( $\pm$ 1 V) and 5.5 V ( $\pm$ 2.75 V).

## 9 APPLICATION AND IMPLEMENTATION

Information in the following applications sections is not part of the Runic component specification, and Runic does not warrant its accuracy or completeness. Runic's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

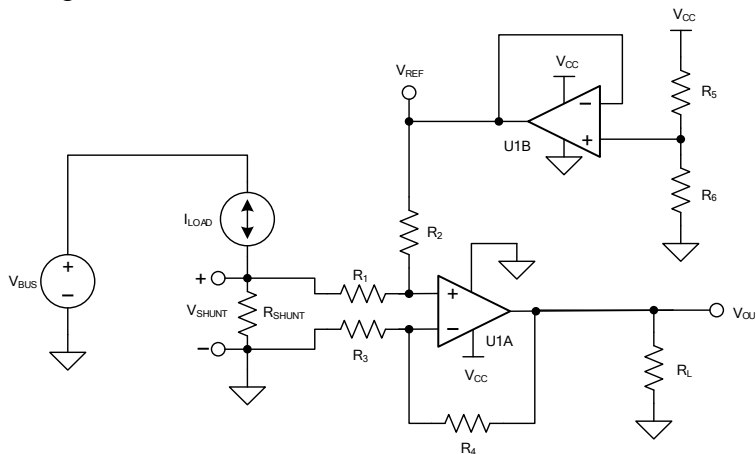
### 9.1 Application Note

The RS854X is a unity-gain stable, precision operational amplifier with very low offset voltage drift; these devices are also free from output phase reversal. Applications with noisy or high-impedance power supplies require decoupling capacitors close to the device power-supply pins. In most cases, 0.1µF capacitors are adequate.

### 9.2 Typical Applications

#### 9.2.1 Bidirectional Current-Sensing

This single-supply, low-side, bidirectional current-sensing solution detects load currents from -1 A to 1 A. The single-ended output spans from 110 mV to 3.19 V. This design uses the RS854X because of its low offset voltage and rail-to-rail input and output. One of the amplifiers is configured as a difference amplifier and the other provides the reference voltage.



**Figure 11. Bidirectional Current-Sensing Schematic**

#### 9.2.2 Design Requirements

This solution has the following requirements:

- Supply voltage: 3.3 V
- Input: -1 A to 1 A
- Output: 1.65 V ±1.54 V (110 mV to 3.19 V)

#### 9.2.3 Detailed Design Procedure

The load current,  $I_{LOAD}$ , flows through the shunt resistor ( $R_{SHUNT}$ ) to develop the shunt voltage,  $V_{SHUNT}$ . The shunt voltage is then amplified by the difference amplifier, which consists of U1A and  $R_1$  through  $R_4$ . The gain of the difference amplifier is set by the ratio of  $R_4$  to  $R_3$ . To minimize errors, set  $R_2 = R_4$  and  $R_1 = R_3$ . The reference voltage,  $V_{REF}$ , is supplied by buffering a resistor divider using U1B. The transfer function is given by Equation 1.

$$V_{OUT} = V_{SHUNT} \times \text{Gain}_{\text{Diff\_Amp}} + V_{REF}$$

Where

$$V_{SHUNT} = I_{LOAD} \times R_{SHUNT}$$

$$\text{Gain}_{\text{Diff\_Amp}} = \frac{R_4}{R_3}$$

$$V_{REF} = V_{CC} \times \left[ \frac{R_6}{R_5 + R_6} \right] \quad (1)$$

There are two types of errors in this design: offset and gain. Gain errors are introduced by the tolerance of the shunt resistor and the ratios of  $R_4$  to  $R_3$  and, similarly,  $R_2$  to  $R_1$ . Offset errors are introduced by the voltage divider ( $R_5$  and  $R_6$ ) and how closely the ratio of  $R_4/R_3$  matches  $R_2/R_1$ . The latter value impacts the CMRR of the difference amplifier, which ultimately translates to an offset error. Because this is a low-side measurement, the value of  $V_{SHUNT}$  is the ground potential for the system load. Therefore, it is important to place a maximum value on  $V_{SHUNT}$ . In this design, the maximum value for  $V_{SHUNT}$  is set to 100 mV. Equation 2 calculates the maximum value of the shunt resistor given a maximum shunt voltage of 100 mV and maximum load current of 1 A.

$$R_{SHUNT(Max)} = \frac{V_{SHUNT(Max)}}{I_{LOAD(Max)}} = \frac{100 \text{ mV}}{1 \text{ A}} = 100 \text{ m}\Omega \quad (2)$$

The tolerance of  $R_{SHUNT}$  is directly proportional to cost. For this design, a shunt resistor with a tolerance of 0.5% was selected. If greater accuracy is required, select a 0.1% resistor or better.

The load current is bidirectional; therefore, the shunt voltage range is -100 mV to 100 mV. This voltage is divided down by  $R_1$  and  $R_2$  before reaching the operational amplifier, U1A. Take care to ensure that the voltage present at the noninverting node of U1A is within the common-mode range of the device. Therefore, it is important to use an operational amplifier, such as the RS854X, that has a common-mode range that extends below the negative supply voltage. Finally, to minimize offset error, note that the RS854X has a typical offset voltage of  $\pm 3\mu\text{V}$  ( $\pm 30\mu\text{V}$  maximum). Given a symmetric load current of -1 A to 1 A, the voltage divider resistors ( $R_5$  and  $R_6$ ) must be equal. To be consistent with the shunt resistor, a tolerance of 0.5% was selected. To minimize power consumption, 10-k $\Omega$  resistors were used. To set the gain of the difference amplifier, the common-mode range and output swing of the RS854X must be considered. Equation 3 and Equation 4 depict the typical common-mode range and maximum output swing, respectively, of the RS854X given a 3.3-V supply.

$$-100\text{mV} < V_{CM} < 3.4\text{V} \quad (3)$$

$$100\text{mV} < V_{OUT} < 3.2\text{V} \quad (4)$$

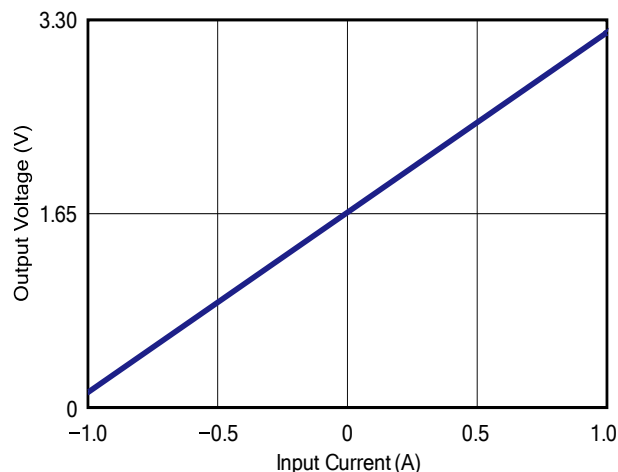
The gain of the difference amplifier can now be calculated as shown in Equation 5.

$$\text{Gain}_{\text{Diff\_Amp}} = \frac{V_{OUT\_Max} - V_{OUT\_Min}}{R_{SHUNT} \times (I_{MAX} - I_{MIN})} = \frac{3.2 \text{ V} - 100 \text{ mV}}{100 \text{ m}\Omega \times [1 \text{ A} - (-1 \text{ A})]} = 15.5 \frac{\text{V}}{\text{V}} \quad (5)$$

The resistor value selected for  $R_1$  and  $R_3$  was 1k $\Omega$ . 15.4k $\Omega$  was selected for  $R_2$  and  $R_4$  because it is the nearest standard value. Therefore, the ideal gain of the difference amplifier is 15.4 V/V.

The gain error of the circuit primarily depends on  $R_1$  through  $R_4$ . As a result of this dependence, 0.1% resistors were selected. This configuration reduces the likelihood that the design requires a two-point calibration. A simple one-point calibration, if desired, removes the offset errors introduced by the 0.5% resistors.

## 9.2.4 Application Curve



**Figure 12. Bidirectional Current-Sensing Circuit Performance: Output Voltage vs Input Current**

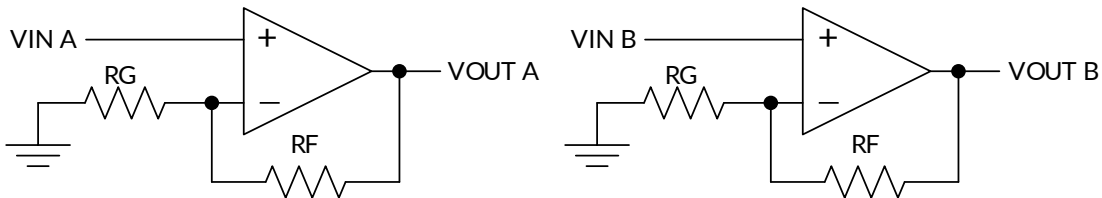
## 10 LAYOUT

### 10.1 Layout Guidelines

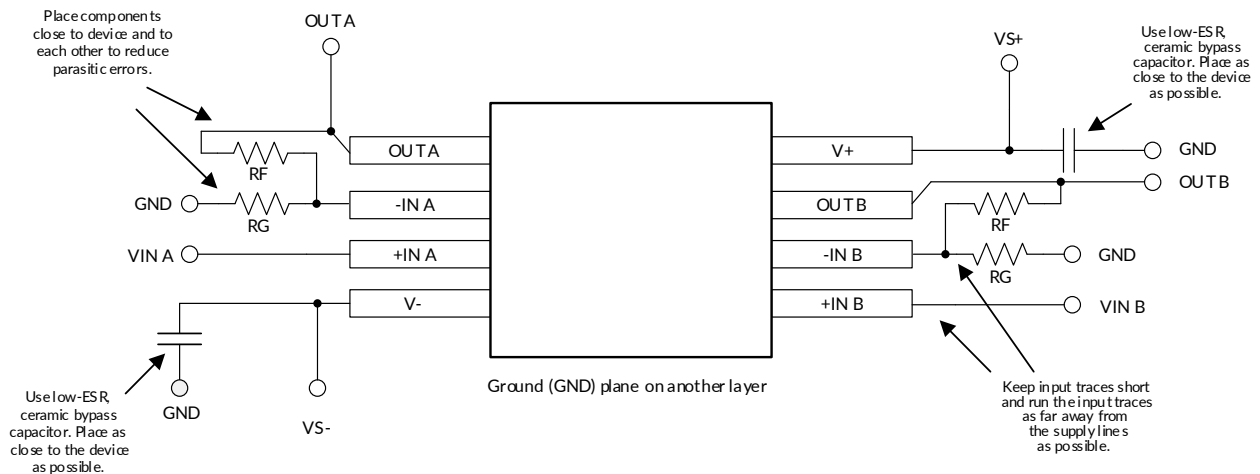
Attention to good layout practices is always recommended. Keep traces short. When possible, use a PCB ground plane with surface-mount components placed as close to the device pins as possible. Place a  $0.1\mu\text{F}$  capacitor closely across the supply pins.

These guidelines should be applied throughout the analog circuit to improve performance and provide benefits such as reducing the EMI susceptibility.

### 10.2 Layout Example



**Figure 13. Schematic Representation**

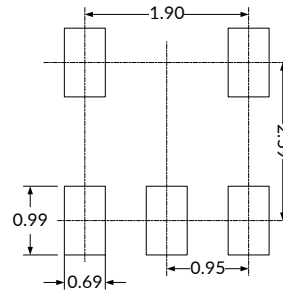
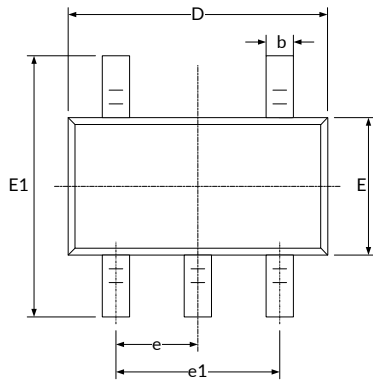
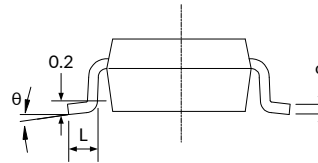
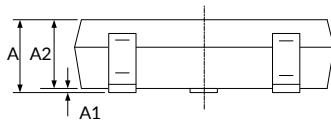


**Figure 14. Layout Example**

NOTE: Layout Recommendations have been shown for dual op-amp only, follow similar precautions for Single and four.

# 11 PACKAGE OUTLINE DIMENSIONS

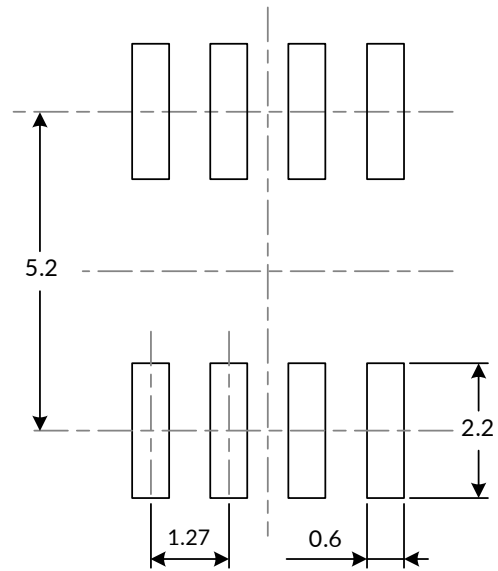
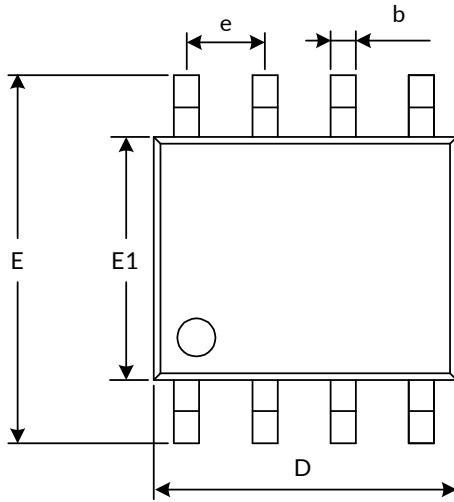
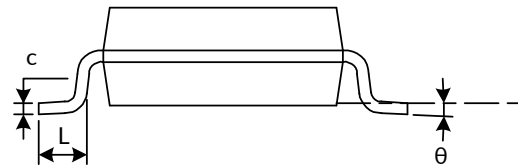
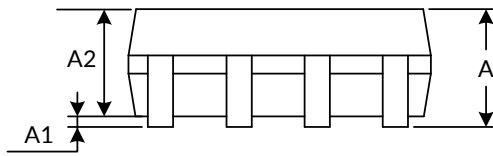
## SOT23-5<sup>(3)</sup>


**RECOMMENDED LAND PATTERN (Unit: mm)**


Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A <sup>(1)</sup>	1.050	1.250	0.041	0.049
A1	0.000	0.100	0.000	0.004
A2	1.050	1.150	0.041	0.045
b	0.300	0.500	0.012	0.020
c	0.100	0.200	0.004	0.008
D <sup>(1)</sup>	2.820	3.020	0.111	0.119
E <sup>(1)</sup>	1.500	1.700	0.059	0.067
E1	2.650	2.950	0.104	0.116
e	0.950(BSC) <sup>(2)</sup>		0.037(BSC) <sup>(2)</sup>	
e1	1.800	2.000	0.071	0.079
L	0.300	0.600	0.012	0.024
$\theta$	0°	8°	0°	8°

**NOTE:**

1. Plastic or metal protrusions of 0.15mm maximum per side are not included.
2. BSC (Basic Spacing between Centers), "Basic" spacing is nominal.
3. This drawing is subject to change without notice.

**SOP8 (3)**

**RECOMMENDED LAND PATTERN (Unit: mm)**


Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A <sup>(1)</sup>	1.350	1.750	0.053	0.069
A1	0.100	0.250	0.004	0.010
A2	1.350	1.550	0.053	0.061
b	0.330	0.510	0.013	0.020
c	0.170	0.250	0.007	0.010
D <sup>(1)</sup>	4.800	5.000	0.189	0.197
e	1.270(BSC) <sup>(2)</sup>		0.050(BSC) <sup>(2)</sup>	
E	5.800	6.200	0.228	0.244
E1 <sup>(1)</sup>	3.800	4.000	0.150	0.157
L	0.400	1.270	0.016	0.050
$\theta$	0°	8°	0°	8°

**NOTE:**

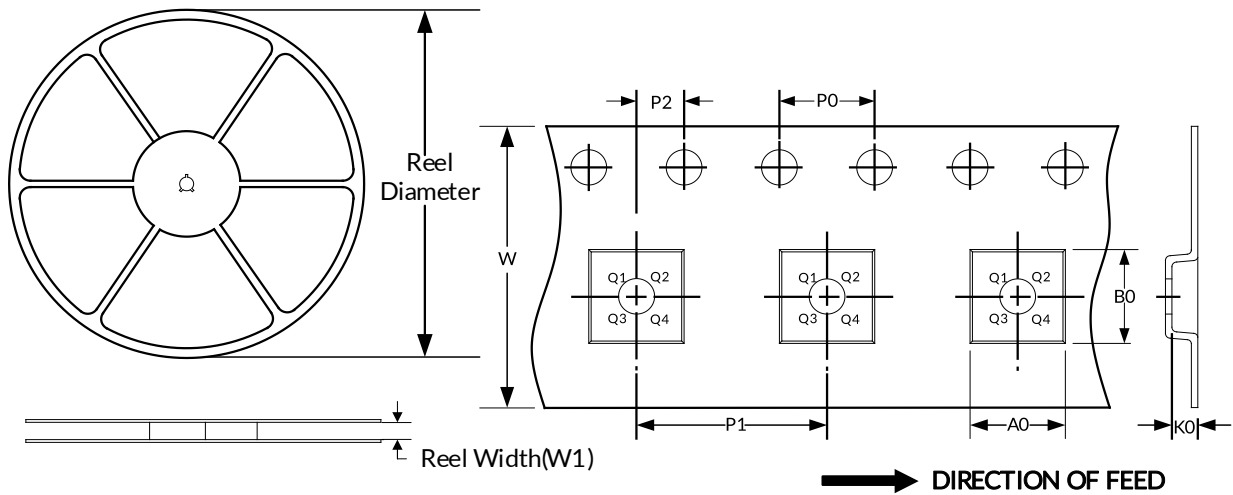
1. Plastic or metal protrusions of 0.15mm maximum per side are not included.
2. BSC (Basic Spacing between Centers), "Basic" spacing is nominal.
3. This drawing is subject to change without notice.



## 12 TAPE AND REEL INFORMATION

### REEL DIMENSIONS

### TAPE DIMENSION



NOTE: The picture is only for reference. Please make the object as the standard.

### KEY PARAMETER LIST OF TAPE AND REEL

Package Type	Reel Diameter	Reel Width(mm)	A0 (mm)	B0 (mm)	K0 (mm)	P0 (mm)	P1 (mm)	P2 (mm)	W (mm)	Pin1 Quadrant
SOT23-5	7"	9.5	3.20	3.20	1.40	4.0	4.0	2.0	8.0	Q3
SOP8	13"	12.4	6.40	5.40	2.10	4.0	8.0	2.0	12.0	Q1

NOTE:

1. All dimensions are nominal.
2. Plastic or metal protrusions of 0.15mm maximum per side are not included.

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